Recovery of Ammonium Metavanadate from Spent Catalyst

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Abstract
Utilization of spent catalysts serves to meet the needs of vanadium and to overcome the environmental problem since vanadium is categorized as a hazardous and toxic material. Vanadium from the spent catalysts can be recovered in the form of $\text{V}_2\text{O}_3$ or NH$_4$VO$_3$. However, vanadate compounds (NH$_4$VO$_3$) are considered to be more valuable due to their higher price and easier production process, compared with $\text{V}_2\text{O}_5$. This study aims to find adequate operating conditions to obtain high yields and high purity of NH$_4$VO$_3$ crystals. The results show that the presence of iron compounds in the extract made the crystals contaminated by brownish colour, so it decreased its purity. Therefore, iron compounds need to be separated first with precipitation. Crystals of NH$_4$VO$_3$ with yield of 60% on spent catalysts and purity of 75% were obtained by extraction using solvent Na$_2$CO$_3$ 1.887 M for 60 minutes at room temperature with weight ratio of V$_2$O$_5$ in spent catalyst toward solvent volume ($R_{sv}$), 0.006 gram V$_2$O$_5$/mL Na$_2$CO$_3$. It was then continued by precipitation of iron compounds at pH of 12 for 2 hours and crystallization of NH$_4$VO$_3$ using NH$_4$Cl 11.215 M for 4 - 5 hours at 60°C.

Keywords: vanadium, vanadate, catalyst, waste, extraction

1. Introduction
Vanadium is a transition metal with many benefits, but its amount is limited. Vanadium level in Earth’s crust is very low, only 0.015% (Kleinberg, et al., 1960). 85% of vanadium is used for metal industry, e.g. in processing titanium alloy and iron. As a catalyst, vanadium serves to make catalysts of dehydrogenation, hydrogenation, alcohol oxidation, dioxide hydrogenation, hydrocarbon oxidation, haloperoxidation, sulphur oxidation, aldehyde/ketone oxidation, and ROMP (Langeslay et al., 2019). One of the most frequently used vanadium oxides in the industry is $\text{V}_2\text{O}_5$. In Indonesia, these compounds are commonly used as catalysts of contact process in sulphate acid production. Besides $\text{V}_2\text{O}_5$, vanadium compound frequently used in industry is ammonium metavanadate (NH$_4$VO$_3$) (Nordberg, 1998). These compounds are used as catalyst, dye, chemical reagent, and ceramic coating (Ayers, et al., 1998).

This need for vanadium keeps increasing, while its availability keeps decreasing. Metal ore has vanadium at small amount (less than 2% or ppm scale) (Nejad et al., 2018). Therefore, it requires innovations to get vanadium. Considering that the main use of vanadium is as catalyst, the spent catalyst is one of potential sources of vanadium. An average use of vanadium catalyst (including regeneration) is 10 years; after this period, the catalyst becomes non-active due to thermal degradation, fouling, and poisoning, so it cannot be used for commercial process (Yin & Finke, 2005). Vanadium catalyst waste belongs to dangerous, toxic waste according to Indonesia Constitution No. 32 Year 2009, so it can lead to environmental problems (Ifa, et al., 2017). Thus, the use of vanadium from spent catalyst is beneficial in terms of economy and useful for prevention of environmental problem (Zeng, et al., 2009).

Recovery process of vanadium from catalyst or metal ore can be performed with pyrometallurgy or hydrometallurgy (Navarro et al., 2007). This process is then continued with crystallization to get a purer product. This process has been developed for recovery of other metals with high values, such as molybdenum from spent catalyst (Kar, et al., 2005). Pyrometallurgy can be done by roasting or direct smelting which requires high temperature (above 300°C to get the best purity) (Kar et al., 2005). On the other hand, leaching/extraction of solvent (with hypochlorite, acid, base, ammonia, or biological agents) (Zhang, et al., 1995) (Zhang, et al., 1996), ion exchange (Li et al., 2009)(Belli Olchini et al., 2012), carbon adsorption (Namasivayam & Sangeetha, 2006), and precipitation (Mazurek, 2013) belong to hydrometallurgy. Although its operating cost is low, precipitation is not


crystallization of model solution 1 was performed by pouring model solution 1 (as model solution 1) and NaCl 11.215 M solution as salting out agent in crystallization of NH₄VO₃.

2.2. Extraction Stage

The first stage of this research was the vanadium extraction from the spent catalyst based on the Rokukawa Method. The extraction was done by stirring in chemical glass of 1 L which contained the spent catalyst with a particle size of 100 mesh, Na₂CO₃ solution (as model solution 1), H₂SO₄ 9 M and NaOH 6 M as pH regulator in the iron precipitation, and NH₄Cl 11.215 M solution as the salting out agent in crystallization of NH₄VO₃.

2.3. Crystallization Stage

The second stage of this research was the crystallization of the model solution based on Baker Method. There were two model solutions to be fed in this stage, namely Na₂CO₃ which only contained V₂O₅ (model solution 1) and Na₂CO₃ solution which contained V₂O₅ and iron compounds (model solution 2).

2.3.1. Crystallization of model solution 1

The crystallization of model solution 1 was performed by pouring model solution 1 which had been heated up to 60°C into a chemical glass which contained the heated solution of NH₄Cl 11.215 M, with a ratio of 1:1. The
crystallization was performed at room temperature and 60°C, with the time variation of 2-6 hours. For the crystallization at room temperature, the chemical glass which contained the model solution and NH₄Cl was placed in a fume hood and left for a certain crystallization time. Meanwhile, for the crystallization at a temperature of 60°C, the chemical glass was placed in a water bath with a temperature that had been set up. The formed crystal was then separated from its solution with a simple filtering method. After that, the crystal was dried and measured until its weight was constant. For the analysis, the dry crystal was dissolved in H₂SO₄ solution with heating. An analysis was conducted in titrimetry to identify vanadium in the crystal.

2.3.2. Crystallization of model solution 2

Before conducting the crystallization, iron compounds in model solution 2 must be reduced/eliminated by precipitation at certain pH for 120 minutes. In this research, the pH of iron precipitation was varied between 2-13. With the initial pH of the solution of around 10, the pH was regulated by adding H₂SO₄ 9 M and NaOH 6 M solutions. After the pH was obtained, the formed solid was precipitated for 120 minutes and separated from its solution with a simple filtering method. The obtained filtrate I was analyzed using titrimetry method to identify the vanadium content and AAS to identify the iron content.

2.3.3. Choosing crystallization method for filtrate

Furthermore, the filtrate for crystallization was chosen based on its iron and vanadium content. The selected filtrate was filtrate with low iron content and high vanadium content. An analysis of the iron and vanadium content was conducted by dissolving dry crystal in H₂SO₄ solution with heating. An analysis of the iron content was conducted with AAS, while the vanadium analysis was performed with titrimetry. A crystallization was conducted to model solution 1 at temperature of 60°C with time variation between 240-480 minutes. The formed crystal was then separated from its solution with a simple filtering method, while its crystal was dried and measured until its weight was constant.

2.4. Crystallization Test on the Spent Catalyst Extract

The test was conducted on an extract of the spent catalyst with Rᵥ of 0.006 gram V₂O₅/ml Na₂CO₃ without H₂O₂ as oxidizer. In this test, iron precipitation was performed only at pH above 10.

2.5. Experimental Variable

This research was conducted with variables as shown in Table 1.

Table 1. Experimental Variable

<table>
<thead>
<tr>
<th>Stage</th>
<th>Variable</th>
</tr>
</thead>
<tbody>
<tr>
<td>Extraction</td>
<td>- Concentration of H₂O₂ in feed: 0; 0.8; 1.6; and 2.4 M</td>
</tr>
<tr>
<td></td>
<td>- Comparison of V₂O₅ weight on solvent volume (Rᵥ): 0.002; 0.004; 0.006; 0.008, and 0.011 gram V₂O₅ / ml Na₂CO₃</td>
</tr>
<tr>
<td>Crystallization of model solution 1</td>
<td>- Crystallization time: 120; 180; 240; 300; 360; 420; and 480 minutes</td>
</tr>
<tr>
<td></td>
<td>- Crystallization temperature: 30 and 60°C</td>
</tr>
<tr>
<td>Crystallization of model solution 2</td>
<td>- pH of iron compounds precipitation: 2 – 13</td>
</tr>
<tr>
<td></td>
<td>- crystallization time NH₄VO₃: 240; 300; 360; 420; and 480 minutes</td>
</tr>
</tbody>
</table>

2.6. Analysis Method

An analysis was conducted on the spent catalyst, model solution, filtrate of iron precipitation result, and NH₄VO₃ crystal. The methodology used was:

1. Gravimetric to determine the content of SiO₂ and Al₂O₃ in the spent catalyst;
2. Titrimetry to determine the content of V₂O₅ and iron (Jones Reduktor) in the spent catalyst and V₂O₅ in spent catalyst extract, model solution, filtrate yield of iron and crystal precipitation, NH₄VO₃;
3. Atomic Absorption Spectrophotometry (AAS) to determine the content of vanadium, iron, aluminum, and sodium in the spent catalyst; the content of vanadium, iron, aluminum, and silica in extract of the spent catalyst and NH₄VO₃ crystal; vanadium and iron in model solution and filtrate yield of iron precipitation.

Solids which were analyzed with titrimetry and spectrophotometry methods must be dissolved in acid solvent or melted with base (NaOH) to be dissolved in acid.
3. Result and Discussion

3.1. Spent Catalyst Analysis

The analysis result of the spent catalyst in contact process from PT Petrokimia Gresik is shown in Figure 1. Vanadium in the spent catalyst is larger than in the titanomagnetite ore (0.08–1.6%-b V₂O₅) which was made as the primary source of vanadium all this time. Therefore, the spent catalyst is highly potential to be a vanadium source. However, this catalyst contains impurities which can affect the quality of yield.

![Figure 1. Composition of the spent catalyst in contact process](image)

3.2. Extraction Stage

Rokukawa Extraction used H₂O₂ solution to oxidize the vanadium compounds with valence under 5 into V₂O₅ based on the reaction in equation 1. This oxidation increased the amount of the extracted vanadium since the compound which can be extracted with Na₂CO₃ solvent was V₂O₅ based on equation 2 (Baker, et al., 1950).

\[
\begin{align*}
V₂O₄ + H₂O₂ & \rightarrow V₂O₅ + H₂O \quad (1) \\
V₂O₅ + Na₂CO₃ & \rightarrow 2 NaVO₃ + CO₂ \quad (2)
\end{align*}
\]

Figure 2 shows that the use of H₂O₂ did not affect the extraction yield, though the added amount of H₂O₂ had been excessive. The use of H₂O₂ 30-90 times of its stoichiometric comparison did not increase the extracted vanadium amount. It was different from a result obtained by Rokukawa (1988) in which the use of H₂O₂ that much can increase the extraction percentage to 80-85%. This shows that the spent catalyst used by Rokukawa still had vanadium compounds with valence under five (Rokukawa, 1988). Meanwhile, the spent catalyst in this research was mostly in V₂O₅, so it did not require additional H₂O₂ solution. Furthermore, this pattern was shown by another research using oxalate acid as the acidic leaching agent for the spent Hydrodesulfurization (HDS) catalyst for 4 hours. At a temperature of 50°C, an addition of H₂O₂ up to 3.0 M increased recovery of all metals (90% Mo, 94% V, 65% Ni and 33% Al) (Mulak et al., 2006).

![Figure 2. Effect of H₂O₂ on V₂O₅ yield](image)

At the extraction stage, V₂O₅ in the spent catalyst was diffused into a Na₂CO₃ solvent due to the concentration gradient. The smaller the weight comparison of V₂O₅ in the spent catalyst on the solvent (Rᵥp) volume, the higher the vanadium extract amount will be. The affordable price of Rᵥp shows that much solvent was used, so the feed became aqueous and made the concentration gradient larger, while the mass transfer rate was quite high. Meanwhile, a large Rᵥp (feed was not aqueous) obtained a small concentration gradient and as the result, its mass transfer rate was low. Thus, when the extraction was done at the same time (60 minutes), amount of V₂O₅ extracted in an aqueous feed was larger than in a dense feed.

![Figure 3. Effect of Rᵥp on yield and concentration of V₂O₅](image)
The extract yielded in this stage was fed for a crystallization stage. The concentration of V$_2$O$_5$ in the extract determined whether or not NH$_4$VO$_3$ was precipitated. In Baker crystallization, the comparison between the NH$_4$Cl solution and the extract (NaVO$_3$ solution) was 1:1. When it was assumed that the whole NaVO$_3$ was converted into NH$_4$VO$_3$, the vanadium concentration in solution at the crystallization process become half of the vanadium concentration in the extract due to the addition of NH$_4$Cl. To make the NH$_4$VO$_3$ precipitated, the NH$_4$VO$_3$ concentration in the solution must be larger than the NH$_4$VO$_3$ solubility in an NH$_4$Cl solution, 0.0094 M V$_2$O$_5$.

Figure 3 shows that when R$_{vp}$ 0.002 gram V$_2$O$_5$/ml Na$_2$CO$_3$ was used (based on what was used by Rokukawara), the obtained vanadium in the extract was 0.011 M V$_2$O$_5$ and its concentration crystallization process was 0.0055 M V$_2$O$_5$. NH$_4$VO$_3$ was not precipitated since this concentration was smaller than the NH$_4$VO$_3$ solubility in NH$_4$Cl. When using R$_{vp}$ 0.004 gram V$_2$O$_5$/ml Na$_2$CO$_3$, the obtained vanadium in the extract was 0.021 M V$_2$O$_5$ and its concentration crystallization process was 0.0105 M V$_2$O$_5$. This concentration was larger than the NH$_4$VO$_3$ solubility in NH$_4$Cl. However, the vanadium compound in this solution decreased due to the impurities elimination in the extract, so the concentration in the crystallization process was expected to decrease up to lower than the NH$_4$VO$_3$ solubility in NH$_4$Cl.

The use of R$_{vp}$ 0.006 gram V$_2$O$_5$/ml Na$_2$CO$_3$ resulted in the extract with a vanadium concentration of 0.030 M V$_2$O$_5$, so its concentration crystallization process was 0.015 M V$_2$O$_5$. This concentration was much larger than the NH$_4$VO$_3$ solubility in NH$_4$Cl, so the solution concentration in the crystallization process decreased below its solubility in the process of extract-polluting compound elimination. Although the use of R$_{vp}$ was larger than 0.006 gram V$_2$O$_5$/ml Na$_2$CO$_3$, it resulted in an extract with a high vanadium concentration at a low extraction percentage, so it was not recommended to be used. Based on these reasons, R$_{vp}$ in this extraction stage was 0.006 gram V$_2$O$_5$/ml Na$_2$CO$_3$. The result of the spent catalyst extraction for 60 minutes with R$_{vp}$ 0.006 gram V$_2$O$_5$/ml Na$_2$CO$_3$ and concentration of Na$_2$CO$_3$ 1.887 M is shown in Table 2.

These values tended to approach a vanadium yield from the spent catalyst of selective catalytic reduction (SCR) with the leaching agent of 2 M NaOH and 0.2 M Na$_2$CO$_3$, and ratio of solid and liquid 1:20, of 86% (Kim et al., 2015). Table 2 shows that the Na$_2$CO$_3$ solvent extracted V$_2$O$_5$ from the spent catalyst and dissolved compounds of iron, aluminum, and silica, but the extracted amount of aluminum and silica was little, so it can be assumed that these two compounds did not affect the yield quality. Meanwhile, iron compounds were extracted at a quite large amount. Although it was smaller than the vanadium concentration, iron was highly influential to the colour of the NH$_4$VO$_3$ crystal since it made the crystal brown. In order to improve the yield quality, in terms of colour and purity, the concentration of iron compounds must be lowered or before crystallization process.

**Table 2. Result of the spent catalyst extraction**

<table>
<thead>
<tr>
<th>Component</th>
<th>Concentration (M)</th>
<th>Yield (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>V$_2$O$_5$</td>
<td>0.03</td>
<td>81.27</td>
</tr>
<tr>
<td>Fe$_2$O$_3$</td>
<td>0.005</td>
<td>42.02</td>
</tr>
<tr>
<td>Al$_2$O$_3$</td>
<td>0.00007</td>
<td>0.42</td>
</tr>
<tr>
<td>SiO$_2$</td>
<td>0.00096</td>
<td>0.07</td>
</tr>
</tbody>
</table>

### 3.3. Crystallization Stage

In this stage, two feed types were used, namely Na$_2$CO$_3$ which contained V$_2$O$_5$ (model solution 1) and a Na$_2$CO$_3$ solution which contained V$_2$O$_5$ and iron compounds (model solution 2). The concentrations of vanadium and iron in feed were in accordance with the extract of the spent catalyst, namely 0.030 M and 0.005 M Fe$_2$O$_3$.

The crystallization of model solution 1 was affected by temperature and the time of crystallization as shown by Figure 4 which indicates that the amount of NH$_4$VO$_3$ crystal yield increased along with the temperature rise. Its reaction speed increased along with the increasing temperature, so the yield increased. Thus, based on the experiment, the crystallization of NH$_4$VO$_3$ should take place at a high temperature, around 60°C.

Figure 4 shows that the amount of the formed NH$_4$VO$_3$ crystal kept increasing, but it tended to be constant after the crystallization more than 360 minutes. At that time, the NH$_4$VO$_3$ crystal yield was quite high, around 93%, which showed that almost all vanadium was crystallized. However, this high yield was not followed by a high purity of NH$_4$VO$_3$ crystal yield. Figure 5 shows that the crystal purity decreased along with the additional time for
crystallization. It was caused by the forming of NH₄Cl crystal as the result of evaporation during the crystallization. It decreased the solution volume, while at a time the NH₄Cl concentration exceeded its solubility in water, so NH₄Cl was crystallized. The existence of NH₄Cl crystal can be identified with white acid when the crystal was heated in a H₂SO₄ solution.

An extraction process cannot be directly performed in model solution 2 since the solution still contained iron. Thus, a reduction/elimination of iron compounds from the solution needed to be performed with precipitation at a certain pH. The effect of pH on the precipitation result is shown in Figure 6. Iron in the filtrate decreased at a pH range of 2-7. It means that Fe²⁺ can be precipitated since its solubility decreased along with pH increase. Fe²⁺ was precipitated as Fe(OH)₂ based on equation 3. On the other hand, iron in the filtrate increased with pH increase from 7 to 9. It shows that the dissolved Fe(OH)₂ sediment became HFeO₂⁻ based on equation 4.

Research shows the result (Figure 6) that iron compound precipitation can be performed in two pH ranges, namely 3.6-8.4 and 11-13.2. However, at pH range of 3.6-8.4, much vanadium compounds were precipitated again as Fe(OH)₂ based on equation 5. Precipitation was started at pH around 10.68 (Pourbaix, 1974).

\[
\text{Fe}^{2+} + \text{H}_2\text{O} \rightarrow \text{Fe(OH)}_2 + 2 \text{H}^+ \quad (3)
\]
\[
\text{Fe(OH)}_2 \rightleftharpoons \text{HFeO}_2^- + \text{H}^+ \quad (4)
\]
\[
\text{HFeO}_2^- + \text{H}_2\text{O} \rightarrow \text{Fe(OH)}_3 + \text{e} \quad (5)
\]

The solubility of HFeO₂⁻ increased along with the pH increase, while its solubility was larger than Fe(OH)₂ for pH above 9. However, at pH above 10, the amount of iron in filtrate decreased. It shows that the iron compounds were precipitated again as Fe(OH)₃ based on equation 5. Precipitation was started at pH around 10.68 (Pourbaix, 1974).
crystallization feed used in this part was model solution 2 in which its iron content has been reduced at pH 12-13.2. This range was different from the precipitation using (NH₄)₂SO₄ which was better at pH 7.2-7.6 (Gladyshev et al., 2015).

The crystallization of model solution 2 was performed at a temperature of 60°C and time variation between 4-8 hours. The crystallization result is shown in Figure 7. The amount of the formed NH₄VO₃ crystal increased along with the increase of crystallization time and it tended to be constant after more than 360 minutes of crystallization. At that time, the yield of NH₄VO₃ crystal of around 82% was recommended for model solution with iron precipitation at pH 12 and 13. This yield was smaller than the crystallization yield of model solution 1 which reached 93% at the same time. Vanadium compounds were also precipitated when reducing/eliminating the iron compounds. Meanwhile, the purity of NH₄VO₃ crystal yield decreased along with the crystallization time, as shown in model solution 1. As previously described, it was caused by the forming of NH₄Cl crystal.

![Figure 7](image)

**Figure 7.** Yield and purity of NH₄VO₃ crystal from model solution 2

In Figure 7, iron precipitation at pH 12 and 13 did not provide a meaningful difference, in terms of the yield and purity of NH₄VO₃ crystal. Therefore, iron compound precipitation was performed at pH 12 since it can result in a colourless filtrate with a tiny iron concentration, namely 1.66 × 10⁻⁵ M Fe₂O₃. In terms of time, the crystallization of model solution 2 should be performed for 4-5 hours since the NH₄VO₃ crystal yield was quite high at that time and the purity was 77.93 %-%, exceeding the commercial NH₄VO₃ (76.73 %-%) purity. Like crystallization of model solution 1, the crystal purity can be improved using a reflux implementation.

3.4. Crystallization on Spent Catalyst Extract

The recovery result of vanadium from the spent catalyst is shown in Figure 8. It shows that the vanadium extracted from the spent catalyst was quite high, around 81.27%. However, this yield decreased into 71.98%, after reduction/elimination of iron compounds from the extract. It means that vanadium compounds were precipitated in the iron precipitation process.

The vanadium yield from the crystal was smaller than in filtrate I. It shows that not all vanadium in filtrate can be crystallized. It was caused by the consideration to stop the crystallization before much NH₄Cl was crystallized again, though there was a possibility that NH₄VO₃ kept increasing. As the result, the NH₄VO₃ crystal yield decreased. Besides, the forming of NH₄Cl decreased the purity of the NH₄VO₃ crystal, so it must be avoided (Figure 8).

![Figure 8](image)

**Figure 8.** Recovery result of vanadium from the spent catalyst

![Figure 9](image)

**Figure 9.** Comparison of crystallization result in model solution 1, model solution 2, and extract of the spent catalyst

As shown in Table 3, vanadium in NH₄VO₃ crystal in the research result was still below the standard of commercial NH₄VO₃ crystal. Meanwhile, compounds of iron, aluminum, and silica were relatively the same with
commercial NH$_4$VO$_3$ crystal. In order to improve the purity in NH$_4$VO$_3$ crystal yield, excess NH$_4$Cl should not crystallize again.

Crystallization test on the spent catalyst extract was conducted by following the crystallization procedure of model solution 2. It was caused by the consideration that the polluting compounds in the spent catalyst extract were only iron compounds. The crystallization was performed at a temperature of 60°C for 5 hours with the extract feed in which iron precipitation was performed at pH 12.

A comparison of the crystallization result in model solution 1, model solution 2, and the extract of the spent catalyst is shown in Figure 9. The NH$_4$VO$_3$ crystal yield from model solution 2 and the spent catalyst extract was smaller than yield in model solution 1. Vanadium compounds were also precipitated when reducing/eliminating the iron compounds. Beside the yield, the crystal purity in model solution 2 and the catalyst extract was lower than in model solution 1 since it had the polluting compounds in the solution. Model solution 2 had iron compounds, while the spent catalyst extract had iron, silica, and aluminum.

Table 3. Composition of NH$_4$VO$_3$ Crystal

<table>
<thead>
<tr>
<th>Component</th>
<th>Composition (%-b)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Research</td>
</tr>
<tr>
<td>V$_2$O$_5$</td>
<td>75.48</td>
</tr>
<tr>
<td>Fe$_2$O$_3$</td>
<td>0.01</td>
</tr>
<tr>
<td>Al$_2$O$_3$</td>
<td>&lt;0.01</td>
</tr>
<tr>
<td>SiO$_2$</td>
<td>&lt;0.10</td>
</tr>
</tbody>
</table>

Table 3 shows a comparison of the NH$_4$VO$_3$ crystal composition in the research result and commercial crystal. The vanadium content from the research was still below the standard of commercial NH$_4$VO$_3$ crystal. Meanwhile, it can be said that the compounds of iron, aluminum, and silica almost met the standard of commercial NH$_4$VO$_3$ crystal. Therefore, to improve the purity of NH$_4$VO$_3$ crystal yield, a recrystallization of NH$_4$Cl excess must be prevented as discussed in previous section.

4. Conclusion

The spent catalyst in contact process of PT Petrokimia Gresik has a potential to be made as a source of vanadium. For the preparation in crystallization stage, the best condition of the extraction stage is a ratio between the V$_2$O$_5$ weight in spent catalyst and the solvent volume of around 0.006 gram V$_2$O$_5$/ml Na$_2$CO$_3$. Iron compounds are the most influential impurities on quality of NH$_4$VO$_3$ crystal yield. Other impurities such as silica and aluminum are relatively negligible. The iron concentration in feed solution at crystallization stage must be reduced with precipitation. In order to get the best result, iron precipitation is performed at a pH of 12. With a crystallization at a temperature of 60°C, the NH$_4$VO$_3$ yield for feed of the spent catalyst extract reached around 75% with a crystal purity of around 76%-b.

References


Zhang, P., Inoue, K., Yoshizuka, K., & Tsuyama, H. (1996). Extraction and selective stripping of molybdenum (VI) and vanadium (IV) from sulphuric acid solution containing aluminium (III), cobalt (II), nickel (II) and iron (III) by LIX 63. Hydrometallurgy, 41, 45-53.